

FacadeMatrix

WIND LOAD & MULLION Ixx CALCULATOR

SAMPLE CALCULATION REPORT

Bengaluru Commercial Tower · IS 875 Part 3:2015 · Free · No login required

REPORT REFERENCE

SR-IS875-001

26 May 2026

Reference Case

Bengaluru · Terrain Category 2 · $h = 45 \text{ m}$ · $b = 1.5 \text{ m}$ · $L = 3.5 \text{ m}$

This sample report is generated for demonstration purposes only. Calculations follow IS 875 Part 3:2015. FacadeMatrix accepts no liability for design decisions made using this sample. Engineers must independently verify all values before use in any submission.

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Input Parameters

City / Location	Bengaluru, Karnataka
ECBC 2017 Climate Zone	Composite
IS 1893 Seismic Zone	Zone II
Design code	IS 875 Part 3:2015
Basic wind speed V_b	33 m/s (IS 875 Part 3 Appendix A)
Risk coefficient k_1	1.00 (50-year return, Cl. 6.3.1)
Terrain Category	Category 2 — open with scattered obstructions
Building class	Class B (50 m > h > 20 m)
k_2 at h = 45 m, TC2 Class B	1.005 (IS 875 Part 3 Table 2, interpolated)
Topography factor k_3	1.00 (flat terrain, Cl. 6.3.3)
Importance factor k_4	1.00 (general buildings, Cl. 6.3.4)
Mean roof height h	45.00 m
Mullion span L	3.50 m
Bay width b	1.50 m

Material Properties — AA 6063-T6 Aluminium

Material	AA 6063-T6 Extruded Aluminium Alloy
Modulus of elasticity E	70,000 MPa (IS 733 / IS 1285)
Yield strength F_y	214 MPa
Allowable bending stress σ_{allow}	128 MPa (ADM ASD · 0.6 x F_y)
Deflection code basis	CWCT TN 32 / AAMA TIR-A11 · L/175 for spans \leq 4.1 m

Code & Standard References

Wind load procedure	IS 875 Part 3:2015 — design wind speed and pressure
Design wind speed	IS 875 Part 3:2015 Cl. 6.3 — $V_z = V_b \times k_1 \times k_2 \times k_3 \times k_4$
Design wind pressure	IS 875 Part 3:2015 Cl. 7.2 — $p_z = 0.6 \times V_z^2$
Pressure coefficients	IS 875 Part 3:2015 Cl. 7.3 — C_{pe} and C_{pi}
Glass design reference	IS 2553 Part 1:2018 — safety glazing
Deflection limit L/175	CWCT TN 32 / AAMA TIR-A11 — spans \leq 4.1 m (13 ft 6 in)
Material standard	IS 733 / IS 1285 — aluminium alloy E = 70,000 MPa
Seismic reference	IS 1893 Part 1:2016 — Zone II (Bengaluru)

Calculation Steps 1–12

Design Wind Speed · Design Wind Pressure · Net Cladding Pressure · Mullion Section Properties

Step 1 — Basic Wind Speed V_b

FORMULA	V_b from IS 875 Part 3:2015 Appendix A — Bengaluru
VALUES	$V_b = 33$ m/s (50-year return period, 3-sec gust equivalent)

RESULT	Vb = 33 m/s
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Step 2 — Risk Coefficient k1

FORMULA	k1 per IS 875 Part 3:2015 Cl. 6.3.1 and Table 1
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VALUES	Design life = 50 years → k1 = 1.00
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RESULT	k1 = 1.00
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Step 3 — Terrain & Height Factor k2

FORMULA	k2 per IS 875 Part 3:2015 Cl. 6.3.2 and Table 2 Terrain Category 2 (TC2) · Building Class B (20 m < h ≤ 50 m)
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VALUES	h = 45 m — interpolating Table 2 TC2 Class B between h=40m (0.988) and h=50m (1.020) $k2 = 0.988 + (1.020 - 0.988) \times (45 - 40) / (50 - 40) = 0.988 + 0.016 = 1.004$
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RESULT	k2 = 1.004 (at h = 45 m, TC2, Class B)
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Table 2 values are for mean hourly wind speed. IS 875:2015 uses these directly for Vz.

Step 4 — Topography Factor k3

FORMULA	k3 per IS 875 Part 3:2015 Cl. 6.3.3
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VALUES	Site is flat — no significant topographic feature within 3 km upwind
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RESULT	k3 = 1.00
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Step 5 — Importance Factor k4

FORMULA	k4 per IS 875 Part 3:2015 Cl. 6.3.4
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VALUES	General commercial office building — cyclone-prone region: No
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RESULT	k4 = 1.00
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Step 6 — Design Wind Speed Vz

FORMULA	$Vz = Vb \times k1 \times k2 \times k3 \times k4$ (IS 875 Part 3:2015 Cl. 6.3)
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VALUES	$Vz = 33 \times 1.00 \times 1.004 \times 1.00 \times 1.00$
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RESULT	Vz = 33.13 m/s
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Step 7 — Design Wind Pressure pz

FORMULA	$pz = 0.6 \times Vz^2$ (IS 875 Part 3:2015 Cl. 7.2)
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VALUES	$pz = 0.6 \times 33.13^2 = 0.6 \times 1,097.6$
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RESULT	pz = 658.6 N/m² = 0.659 kN/m²
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Step 8 — Pressure Coefficients Cpe and Cpi

FORMULA	Cpe per IS 875 Part 3:2015 Cl. 7.3 — external walls Cpi per IS 875 Part 3:2015 Cl. 7.3.2 — enclosed building
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VALUES	Cpe (field zone, suction) = -0.8 Cpe (corner zone) = -1.0 Cpi (enclosed building) = +0.2 (worst case for suction combination)
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RESULT	Cpe field = -0.8 Cpe corner = -1.0 Cpi = +0.2
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Step 9 — Net Design Wind Pressure p_net

FORMULA	$p_{net} = p_z \times (C_{pe} - C_{pi})$ (IS 875 Part 3:2015 Cl. 7.3)
VALUES	Field zone: $p_{net} = 0.659 \times (-0.8 - (+0.2)) = 0.659 \times 1.0 = 0.659 \text{ kN/m}^2$ Corner zone: $p_{net} = 0.659 \times (-1.0 - (+0.2)) = 0.659 \times 1.2 = 0.791 \text{ kN/m}^2$
RESULT	p_design = 0.791 kN/m² (corner zone suction governs) <i>Suction (outward pressure) governs mullion design. Corner zone taken as design case.</i>

Step 10 — Mullion Line Load w

FORMULA	$w \text{ [N/mm]} = p_{design} \text{ [kN/m}^2] \times b \text{ [m]}$ (1 kN/m = 1 N/mm exactly)
VALUES	$w = 0.791 \times 1.50$
RESULT	w = 1.187 kN/m = 1.187 N/mm

Step 11 — Bending Moment and Shear Force

FORMULA	$M = w \times L^2 / 8$ (simply supported · UDL) $V = w \times L / 2$
VALUES	$M = 1.187 \times 3,500^2 / 8 = 1.187 \times 12,250,000 / 8 = 1,818,531 \text{ N}\cdot\text{mm}$ $V = 1.187 \times 3,500 / 2 = 2,077 \text{ N}$
RESULT	M = 1,818,531 N·mm = 1.819 kN·m V = 2,077 N = 2.077 kN

Step 12 — Required Section Modulus Z_req

FORMULA	$Z_{req} = M / \sigma_{allow}$ [$\sigma_{allow} = 128 \text{ MPa} \cdot \text{ADM ASD} \cdot 0.6 \times F_y$]
VALUES	$Z_{req} = 1,818,531 / 128$
RESULT	Z_req = 14,207 mm³ = 14.2 cm³ <i>Select extrusion with section modulus $Z \geq 14,207 \text{ mm}^3$ about the strong axis.</i>

Required Moment of Inertia Ixx — Three Deflection Limits

Common formula: $I_{xx_req} = 5 \times w \times L^4 / (384 \times E \times \delta_{allow})$ where $E = 70,000 \text{ N/mm}^2$ (IS 733 / IS 1285) · all in N and mm.

Step 13 — Ixx at L/175 — Recommended ($L \leq 4.1 \text{ m}$ · CWCT TN 32 / AAMA TIR-A11)

FORMULA	$\delta_{allow} = L/175 = 3,500/175 = 20.00 \text{ mm}$
VALUES	$I_{xx} = 5 \times 1.187 \times 3,500^4 / (384 \times 70,000 \times 20.00)$ $= 5 \times 1.187 \times 1.5006 \times 10^{13} / 537,600,000$
RESULT	Ixx = 1,660,000 mm⁴ = 166.0 cm⁴ ← RECOMMENDED

Step 14 — Ixx at L/240 + 6.35 mm — Long-span limit (CWCT TN 32 / AAMA TIR-A11)

FORMULA	$\delta_{allow} = 3,500/240 + 6.35 = 14.583 + 6.35 = 20.933 \text{ mm}$
VALUES	$I_{xx} = 5 \times 1.187 \times 3,500^4 / (384 \times 70,000 \times 20.933)$
RESULT	Ixx = 1,587,000 mm⁴ = 158.7 cm⁴ <i>L/240+6.35 governs for spans 4.1 m to 12 m. At L=3.5 m, L/175 governs.</i>

Step 15 — Ixx at L/360 — Project-specific (SSG / structurally bonded glazing)

FORMULA	$\delta_{allow} = 3,500/360 = 9.722 \text{ mm}$
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VALUES	$I_{xx} = 5 \times 1.187 \times 3,500^4 / (384 \times 70,000 \times 9.722)$
RESULT	$I_{xx} = 3,419,000 \text{ mm}^4 = 341.9 \text{ cm}^4$

Specify L/360 only when project specification requires it (SSG facades, brittle finishes).

Deflection Limit Summary — AA 6063-T6 Mullion

Deflection Limit	delta_allow (mm)	Ixx required (cm ⁴)	Note
L / 175	20.00	166.0	RECOMMENDED
L / 240 + 6.35 mm	20.93	158.7	
L / 360	9.72	341.9	PROJECT-SPECIFIC

Results Summary

Basic wind speed Vb	33 m/s (Bengaluru · IS 875 Part 3 Appendix A)
Design wind speed Vz (h = 45 m)	33.13 m/s
Design wind pressure pz	0.659 kN/m ²
Governing net pressure p_design	0.791 kN/m ² — corner zone suction governs
Mullion line load w	1.187 kN/m = 1.187 N/mm
Maximum bending moment M	1.819 kN-m
Maximum shear force V	2.077 kN
Required section modulus Z_req	14,207 mm ³ (14.2 cm ³)
Ixx at L/175 (RECOMMENDED)	166.0 cm ⁴
Ixx at L/240 + 6.35 mm	158.7 cm ⁴
Ixx at L/360 (project-specific)	341.9 cm ⁴

Design Recommendation

Select an AA 6063-T6 extruded aluminium mullion with $I_{xx} \geq 166.0 \text{ cm}^4$ (L/175 · CWCT TN 32 · recommended for spans ≤ 4.1 m) and section modulus $Z \geq 14,207 \text{ mm}^3$. Apply 0.791 kN/m² for corner zones. Apply 0.659 kN/m² for field zones. This report uses IS 875 Part 3:2015 with Terrain Category 2, Class B, for a 45 m commercial tower in Bengaluru.

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